

# UK Patent Application GB 2 189 621 A

(43) Application published 28 Oct 1987

(21) Application No 8705066

(22) Date of filing 4 Mar 1987

(30) Priority data

(31) 61/049408 (32) 6 Mar 1986 (33) JP  
61/173091 23 Jul 1986

(51) INT CL<sup>4</sup>  
G02B 6/12

(52) Domestic classification (Edition I):  
G2J GDB

(56) Documents cited  
None

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(58) Field of search  
G2J  
Selected US specifications from IPC sub-class G02B

## (54) Optical demultiplexer and/or multiplexer

(57) A demultiplexing and/or multiplexing optical circuit comprises a substrate (10) having formed therein a branched optical waveguide and a groove (30) for receiving a filter (40) in the optical waveguide (22). The groove (30) is arranged to be perpendicular to a pair of parallel opposing sides (11,12) of the substrate. Because the groove (30) for receiving the filter (40A) adjacent a branched portion is perpendicular to the sides (11,12) a column of demultiplexers and/or multiplexers can be formed simultaneously, and a high machining precision may be achieved relatively easily.

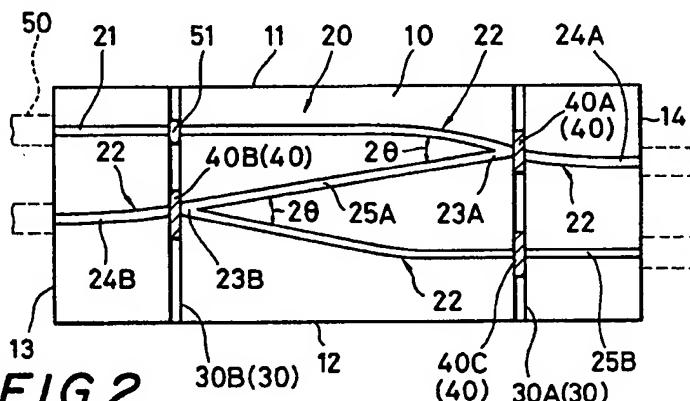


FIG. 2

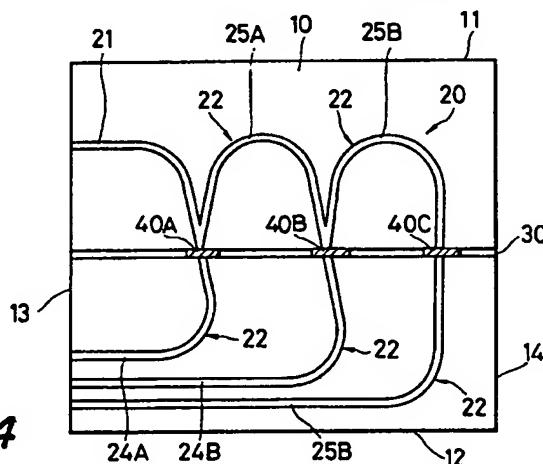


FIG. 4

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FIG. 1

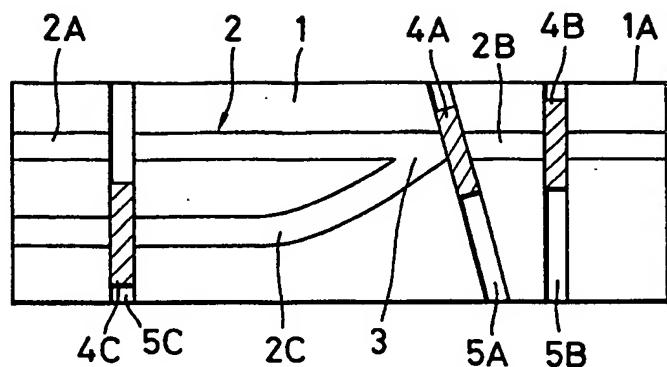
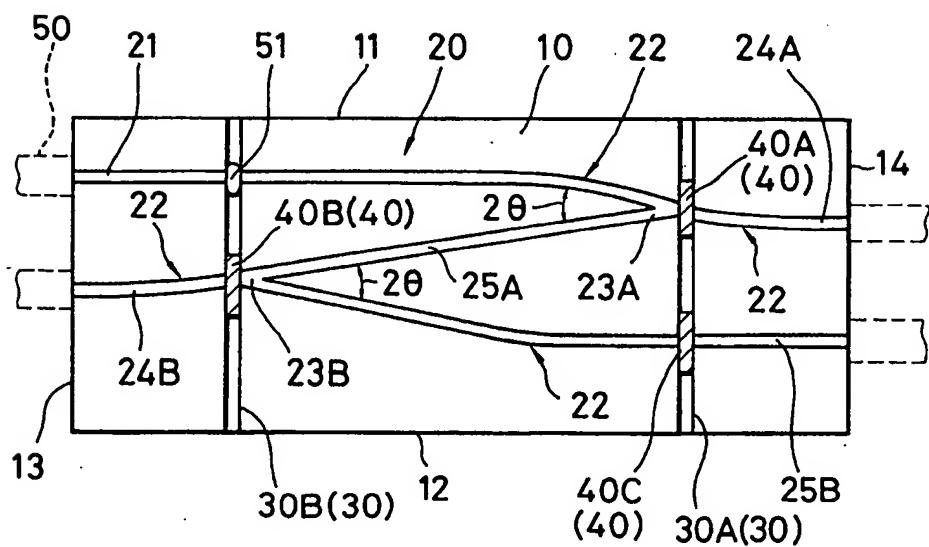


FIG. 2



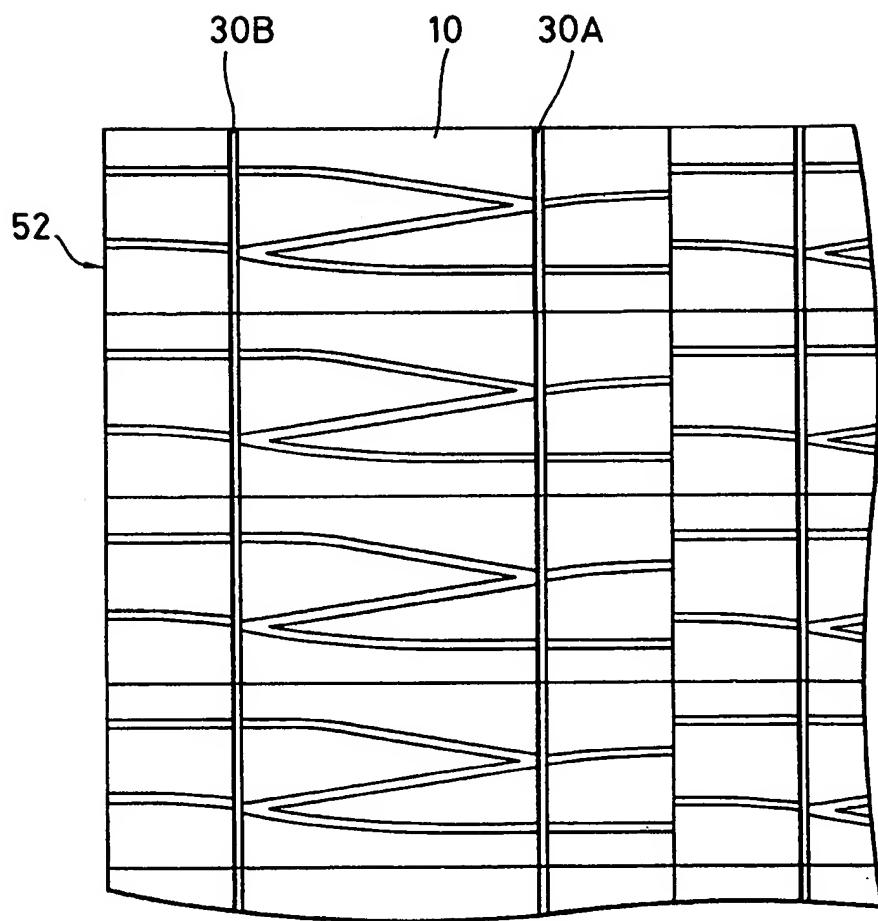
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*FIG. 3*



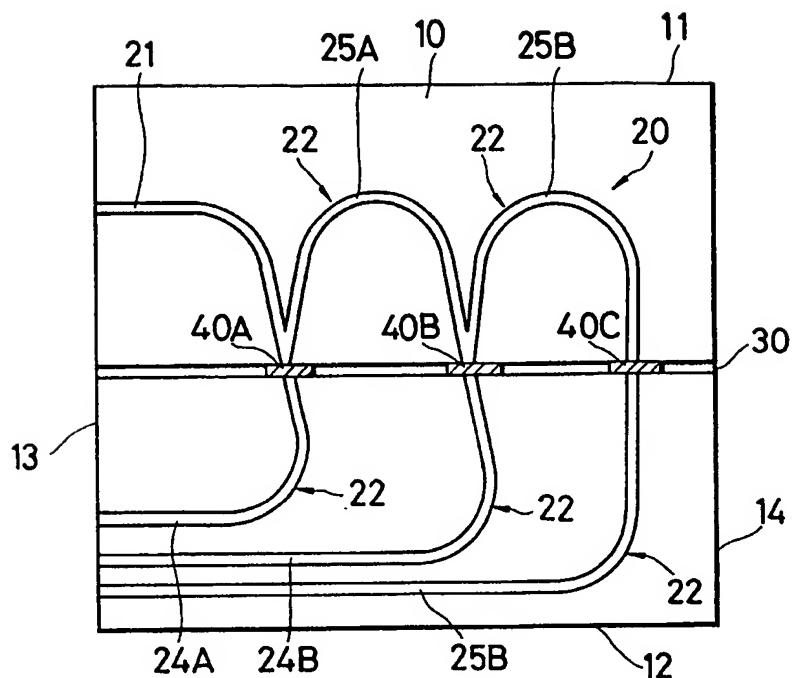
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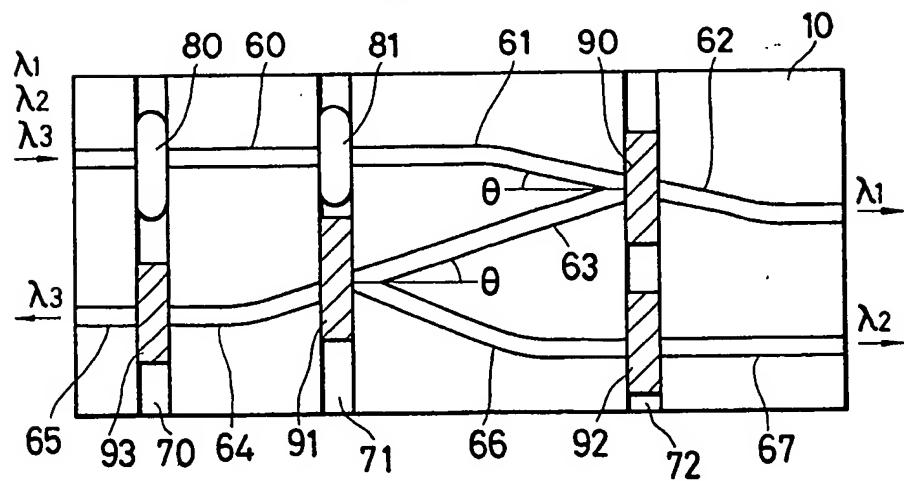
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*FIG. 4*



*FIG. 5*



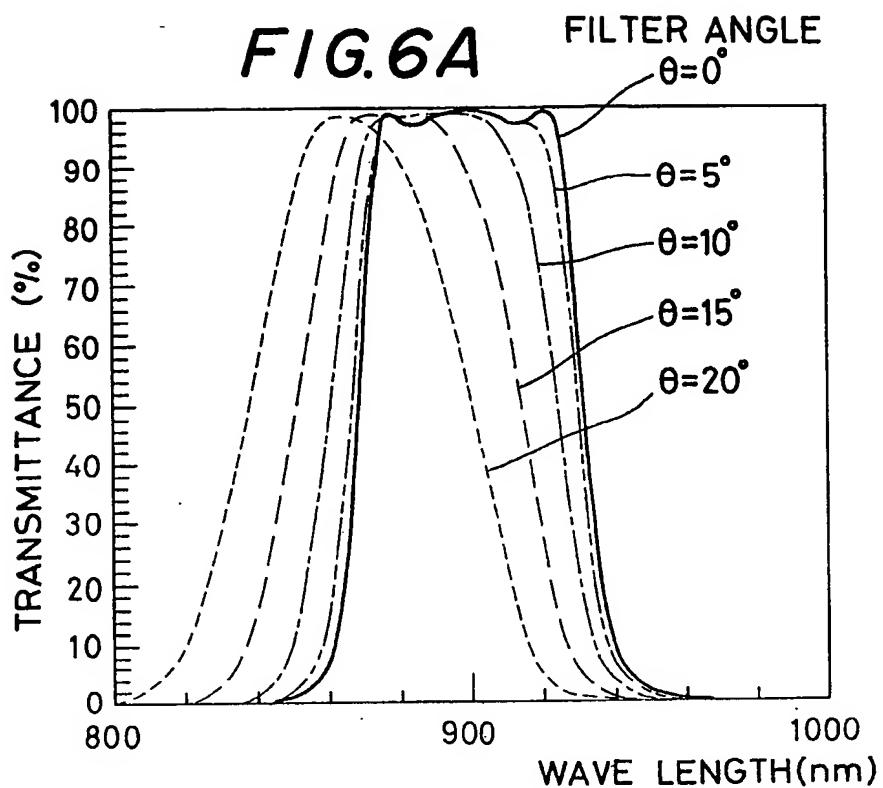
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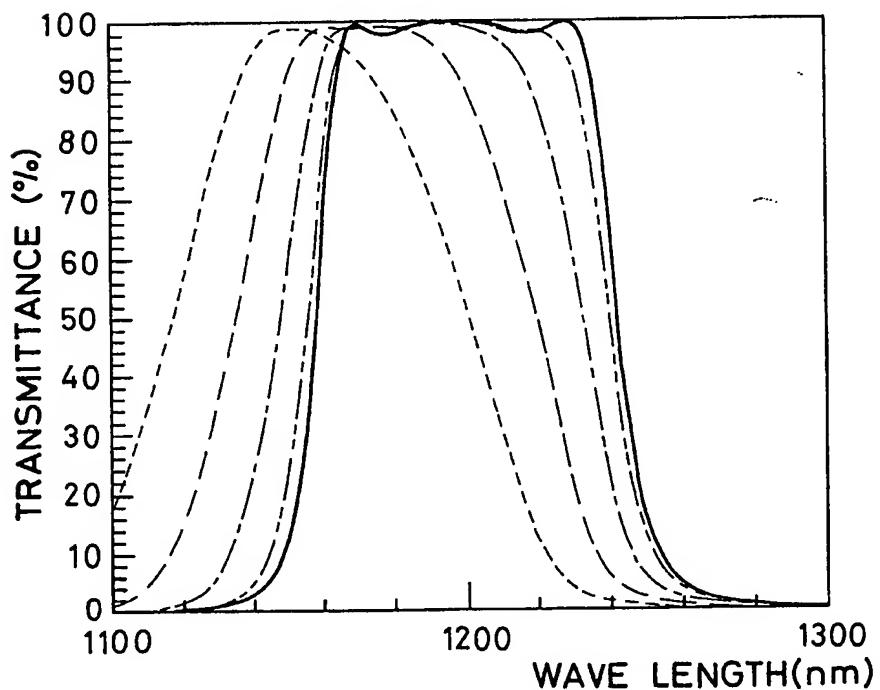
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**FIG. 6A**



**FIG. 6B**



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FIG. 7A

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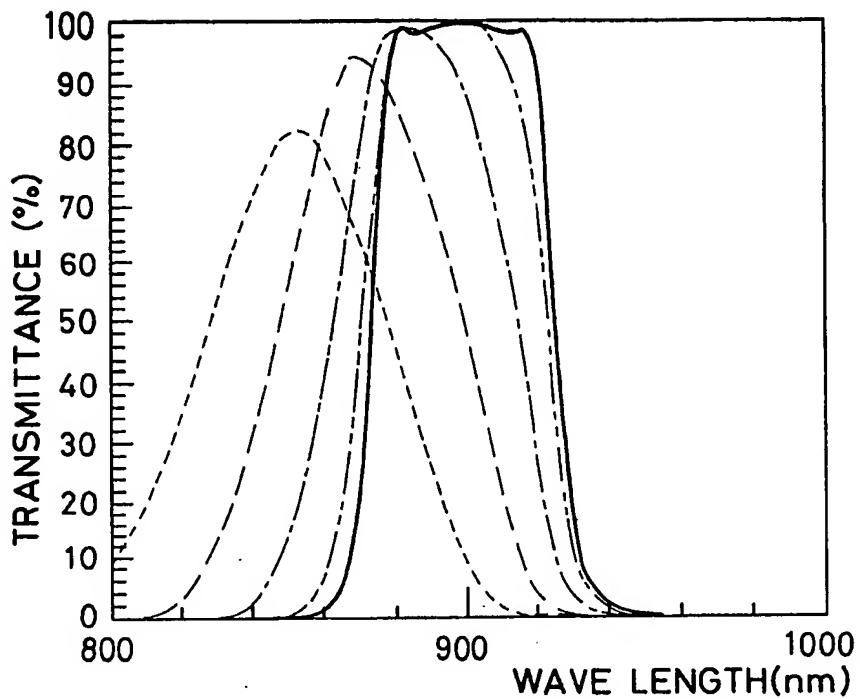
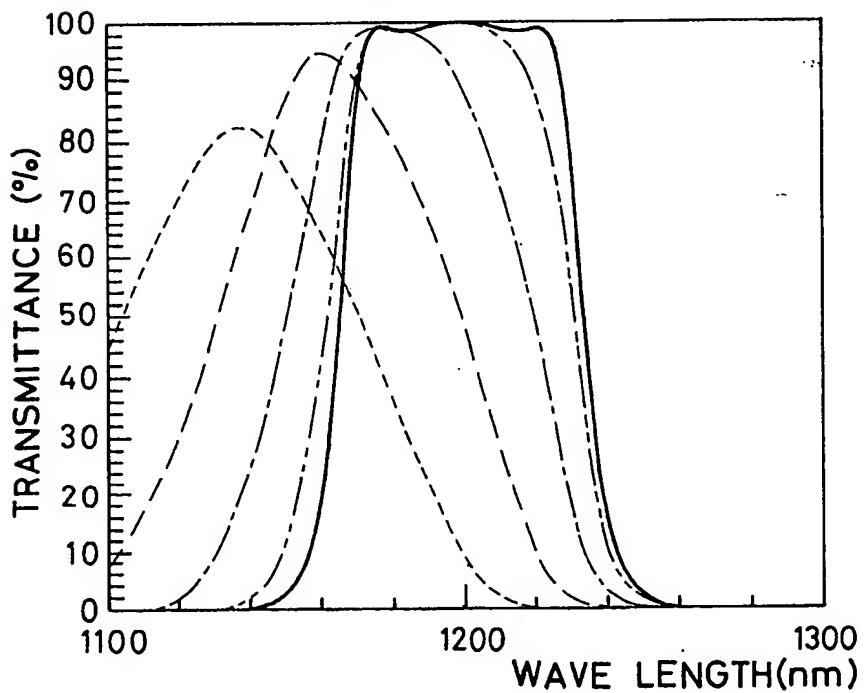


FIG. 7B

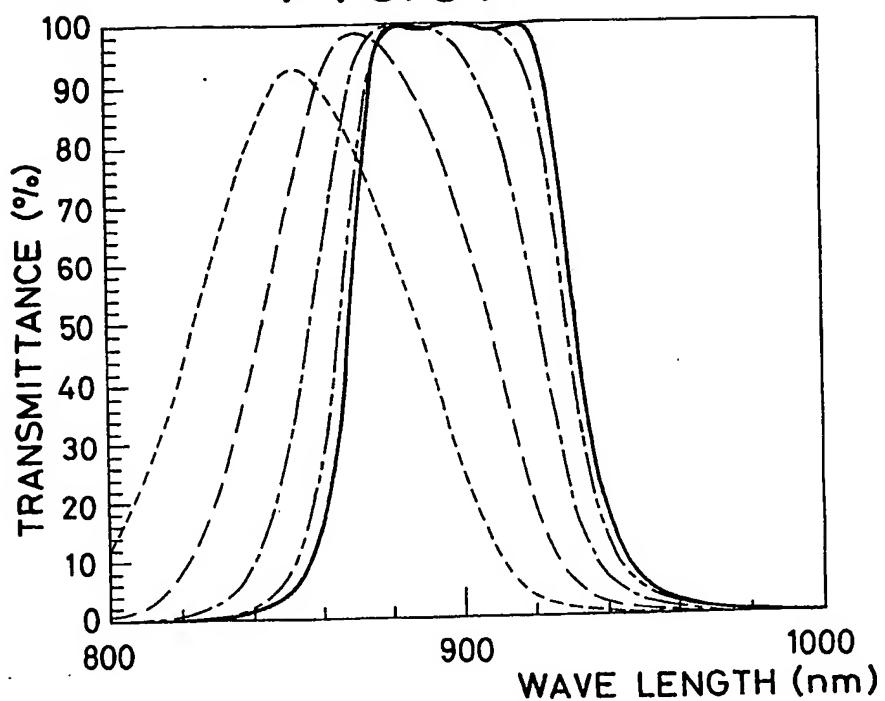


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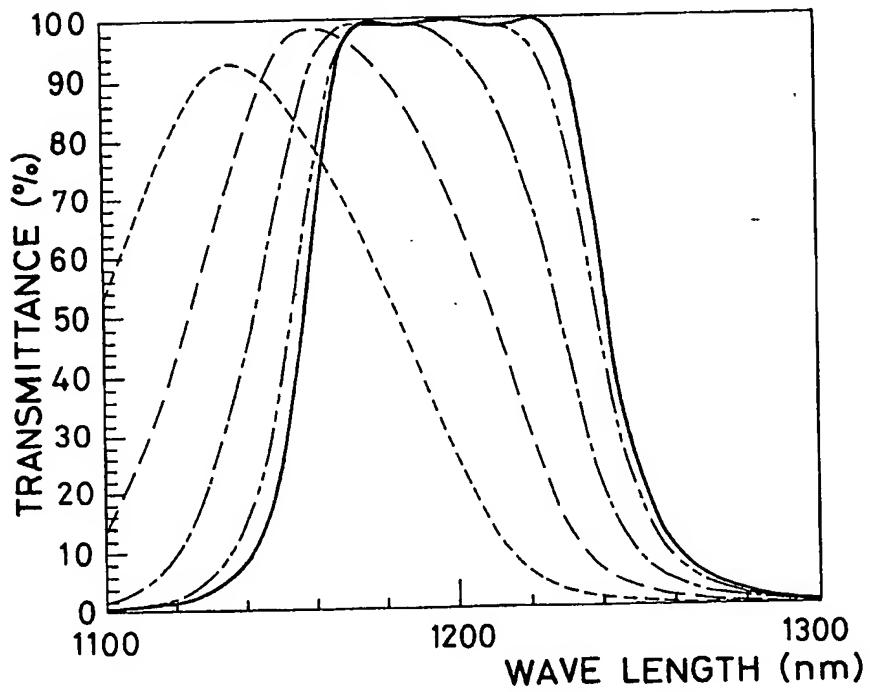
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**FIG. 8A**



**FIG. 8B**



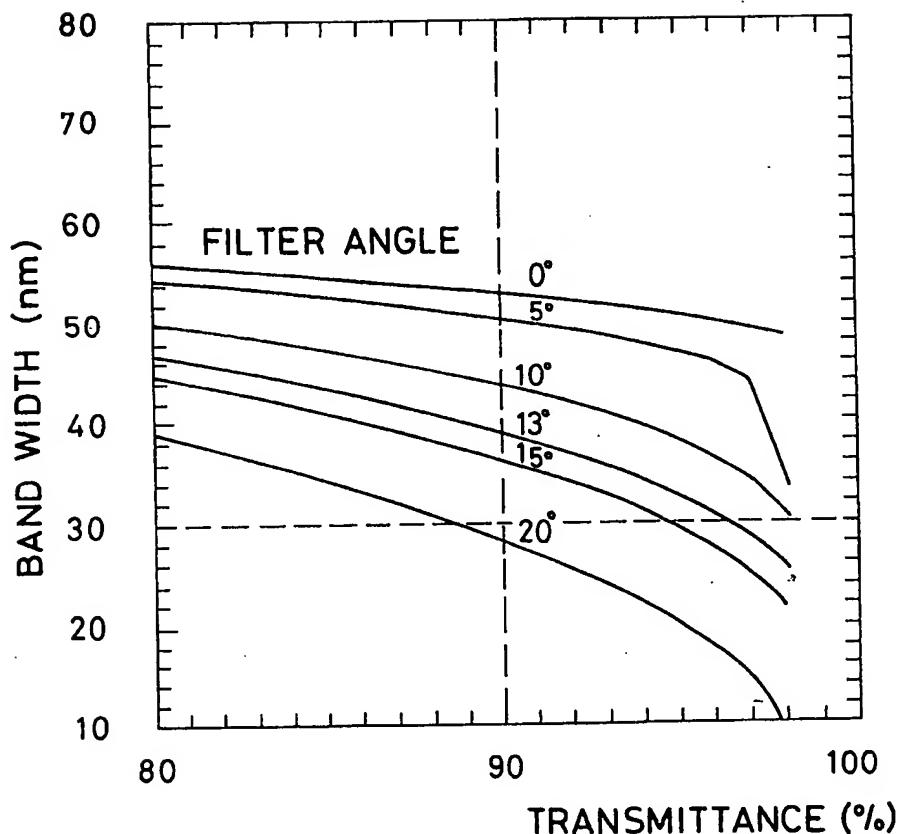
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FIG. 9A



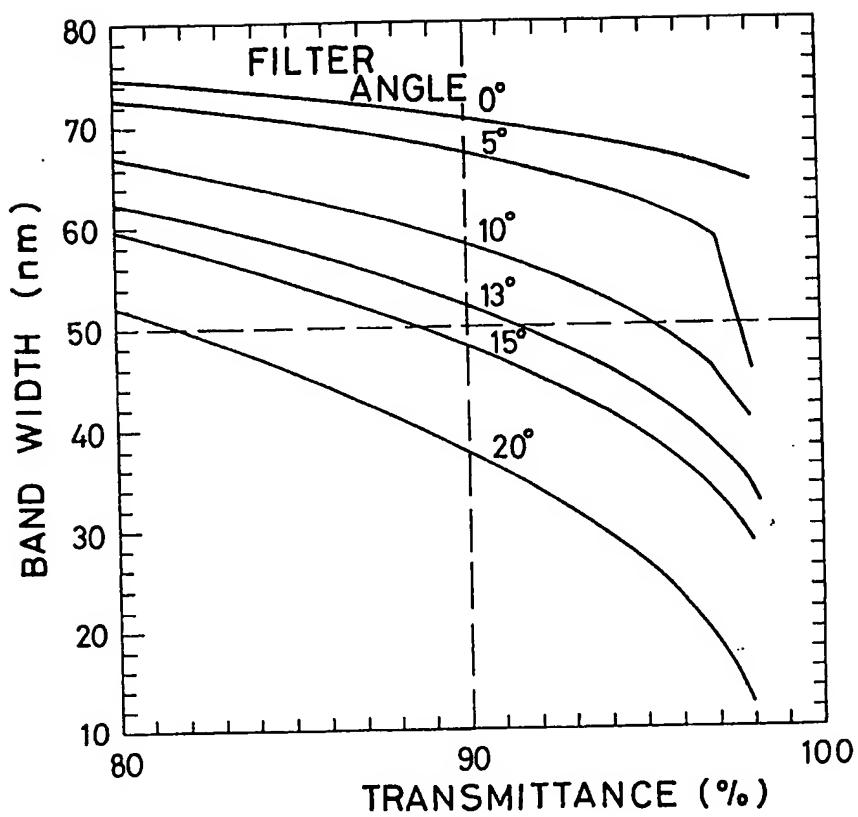
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**FIG. 9B**



## SPECIFICATION

## Optical demultiplexer and/or multiplexer

5 The present invention relates to an optical circuit for use as a demultiplexer and/or multiplexer and in particular, but not exclusively, for such a circuit for use in a wavelength-division multiplexing optical fiber communication system. 5

10 A conventional demultiplexing and/or multiplexing optical circuit of the type using a buried waveguide has a circuit configuration as shown in Fig. 1 of the accompanying drawings. For example, reference is made to the Institute of Electronics and Communication Engineers of Japan, "Characteristics of Guided-wave Multi-/Demultiplexer with Embedded Waveguides by Ion-Exchange Process", *Shingaku giho*, OQE86-1, 1986, pp. 1 to 8. 10

15 Referring to Fig. 1 of the accompanying drawings, an optical waveguide 2 is formed by, e.g., an ion exchange method in a transparent substrate 1 made of e.g., glass. The optical waveguide 2 has a higher refractive index than that of the transparent substrate 1. The optical waveguide 2 has an incident path 2A having one end at one side of the substrate 1, a transmitted light output path 2B, and a reflected light output path 2C branching from the incident path 2A at a branch portion 3. A demultiplexing filter 4A which passes (or reflects) a light of a specific wavelength and reflects (or passes) light of other wavelengths is fitted in the branch portion 3. Bandpass filters 4B and 4C which pass light of specific wavelengths are fitted in transmitted and reflected light output paths 2B and 2C, respectively. 15

20 Grooves 5A, 5B and 5C are formed in the substrate 1 to cross the optical waveguide 2 at the branch portion 3 and at portions partway along the output paths 2B and 2C. The filters 4A, 4B and 4C are fitted in the grooves 5A, 5B and 5C. 20

25 Of these filters, the demultiplexing filter 4A is arranged such that the angle defined by the incident path 2A and the reflected light output path 2C is bisected by a line normal to the surface of the filter 4A. 25

30 In the optical circuit having the above arrangement, assume that a beam including two different wavelengths  $\lambda_1$  and  $\lambda_2$  is passed along the incident path 2A via an optical fiber or the like. Then, only that component of the beam of wavelength  $\lambda_1$  passes through the filter 4A at the branching portion 3, and the components having wavelengths other than  $\lambda_1$  are rejected by the filter 4B to ensure demultiplexing. The component of wavelength  $\lambda_1$  is output from the substrate 1 through the transmitted light output path 2B. The component of wavelength  $\lambda_2$  that has been reflected by the demultiplexing filter 4A at the branch portion 3 passes along the reflected light output path 2C and is output from the substrate 1 after wavelengths other than  $\lambda_2$  are rejected by the filter 4C. 30

35 In the conventional demultiplexing and/or multiplexing optical circuit described above, the incident and transmitted light output paths 2A and 2B are formed parallel to a side 1A of the substrate 1. Thus, the groove 5A for receiving the demultiplexing filter 4A must be inclined with respect to the side 1A of the substrate 1. 35

40 Because the groove 5A in substrate 1 for receiving the filter 4A is inclined with respect to the side 1A of the substrate 1, it must be machined independently for each substrate and this results in a cumbersome operation and poor productivity. 40

45 Besides, it is hard to precisely form inclined grooves on a substrate. If the angles of the fabricated grooves are not correct, the additional losses as at branching portions will increase considerably. The yield of demultiplexing and/or multiplexing optical circuits will inevitably decrease, and optical circuits having stable qualities cannot be obtained with the conventional type of demultiplexer/multiplexer described above. 45

50 The applicants have found that it is possible to provide a stable-quality demultiplexing and/or multiplexing optical circuit in which the above-described conventional problems are solved, which can be machined easily, and which is thus suitable for mass production. 50

55 According to this invention there is provided a demultiplexing and/or multiplexing optical circuit comprising a substrate having two opposed parallel edge regions, an optical waveguide formed in said substrate and including a branched portion for dividing an incident optical path into a transmitting optical path and a reflecting optical path, a groove formed in said substrate in a direction perpendicular to said edge regions and disposed to cross said optical waveguide at said branched portion and at a portion partway along one of said optical paths, and a plurality of filters located in said groove. 55

60 In this case, considering the connecting operability and coupling loss of optical fibers, it is preferable that an arcuate bent portion is provided at an appropriate portion of the optical path so that the optical axis of the optical path at its end is perpendicular to the end of the substrate. 60

65 The invention will now be described by way of example, reference being made to the accompanying drawings, in which: 65

65 Figure 1 is a plan view of an example of a conventional demultiplexing and/or multiplexing

optical circuit;

Figure 2 is a plan view of a demultiplexing and/or multiplexing optical circuit according to a first embodiment of the present invention;

Figure 3 is a plan view showing an intermediate step in the manufacture of the demultiplexing and/or multiplexing optical circuit of Fig. 2;

Figure 4 is a plan view showing a demultiplexing and/or multiplexing optical circuit according to a second embodiment of the present invention;

Figure 5 is a plan view showing a demultiplexing and/or multiplexing optical circuit according to a third embodiment of the present invention;

Figures 6A to 8B are graphs showing wavelength characteristics of three types of filters having different layer configurations; and

Figures 9A and 9B are graphs showing the relationship between the transmittance and the band width of one type of the filters described above.

The first to third embodiments of the present invention will now be described in detail with reference to the accompanying drawings.

Referring to Fig. 2, the circuit includes a substrate 10, an optical waveguide 20, filter-fitting grooves 30, and interference filters 40. The substrate 10 constitutes a rectangle having opposing sides 11 and 12 parallel to each other and opposing ends 13 and 14 parallel to each other.

The optical waveguide 20 is formed by a known optical waveguide forming method, such as two-step ion exchange on a glass substrate 10 or soot deposition on an Si substrate 10. Fig. 2 shows a circuit pattern having three-wave demultiplexing and/or multiplexing functions.

The optical waveguide 20 has an incident path 21 parallel to the side 11 of the substrate 10. The incident path 21 extends to a first branching portion 23A through an arcuate bent portion 22 and is branched into first transmitted and reflected light output paths 24A and 25A. After passing the bent portion 22, the transmitted light output path 24A extends parallel to the side 11 of the substrate 10 and reaches the other end 14 of the substrate 10.

The first reflected light output path 25A extends to a second branching portion 23B and is branched into second transmitted and reflected light output paths 24B and 25B. The output paths 25A and 25B extend obliquely with respect to the sides 11 and 12 of the substrate 10 and become parallel to the sides 11 and 12 of the substrate 10 near the ends 13 and 14, respectively, after they pass corresponding bent portions 22. Hence, the optical paths of the output paths 25A and 25B at the output ends are perpendicular to the ends 13 and 14 of the substrate 10.

The distance between the incident path 21 and the second transmitted light output path 24B at one end 13 of the substrate 10 is set to be equal to that between the first transmitted light output path 24A and the second reflected light output path 25B at the other end 14. The end of each of the incident path 21 and the respective output paths 24A, 24B, and 25B is connected to an optical fiber 50, or is directly connected to a light-emitting or light-receiving element.

Two filter-fitting grooves 30 are formed to extend along the entire width of the substrate 10 to be perpendicular to the sides 11 and 12 of the substrate 10. The sectional size of each groove 30 is, e.g., a width of 50  $\mu\text{m}$  and a depth of 200  $\mu\text{m}$ , so that its width is substantially the same as that of a filter to be used and that its bottom is located under the lower end of the optical waveguide 20.

One groove 30A crosses the optical waveguide 20 at the first branching portion 23A and a portion midway along the second reflected light output path 25B. At the branching portion 23A, the incident path 21 and the reflected light output path 25A each form a constant angle  $\theta$  with respect to the normal to the groove 30A. The second reflected light output path 25B and the groove 30A cross at a right angle.

The other filter-fitting groove 30B crosses the optical waveguide 20 at the second branching portion 23B and at a portion midway along the incident path 21. The angles defined by the optical waveguide 20 and the groove 30B are similar to those defined in the above-described case.

At the first branching portion 23A, a first demultiplexing filter 40A, e.g., a short-wavelength pass interference filter, is fitted and adhered in the groove 30A to cover the section of the optical waveguide 20. Similarly, a filter 40C for cutting the noise of output light, e.g., a 1.2- $\mu\text{m}$  bandpass filter having 35 layers, is fitted in the groove 30A at a portion across the second reflected light output path 25B. Regarding the other groove 30B, a second demultiplexing filter 40B, e.g., a 1.3- $\mu\text{m}$  bandpass filter having 23 layers, is fitted at the second branch portion 23B.

No filter need be fitted in a portion of the incident path 21 at which the groove 30B crosses. Therefore, a optical adhesive 51 having the same refractive index as that of the optical waveguide 20 is filled in the groove 30B so as to optically connect the optical waveguide 20 separated at this portion.

In the above optical circuit, if each bent portion 22 of the optical waveguide 20 has too small a radius of curvature, a radiation loss results. Therefore, it is preferable that the radius of

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curvature is 5 mm at minimum, and more preferably within a range of 10 to 25 mm considering miniaturization of the circuit. If the angles  $\theta$  defined by the incident and reflected output paths at both branching portions 23A and 23B are set to be about  $20^\circ$ , good filter characteristics can be obtained.

5 The optical circuit of the first embodiment having the above arrangement can be efficiently manufactured as shown in Fig. 3. More specifically, a plurality of optical waveguides having predetermined circuit patterns are formed in a large substrate base 52 made of, e.g., glass. Filter-fitting grooves 30A and 30B are formed to extend from one end to the other of the base 52 by a machining means such as a dicing saw. Then, the base 52 is cut into substrate 10 members corresponding to respective circuit substrates 10. 5

10 When the present invention is practiced, it is preferable that the circuit pattern is designed such that the number of portions for cutting the optical waveguide 20 by the grooves 30, other than the portions for receiving the filters 40, is minimized. 10

For example, the circuit pattern can be designed as the second embodiment shown in Fig. 4. 15 More specifically, according to the second embodiment, the incident path 21 and output paths 24A, 24B, and 25B all have inlet/outlet portions which are parallel to sides 11 and 12 of the substrate 10. A groove 30 is also parallel to the sides 11 and 12 of the substrate 10. Bent portions 22 are formed in the optical waveguide 20 to bend it substantially through  $180^\circ$  and  $90^\circ$ . As a result, the groove 30 crosses only a portion of the optical waveguide 20 for receiving 20 filters 40, and the optical axis of the inlet/outlet portions of each of optical paths 21, 24A, 24B and 25B, are perpendicular to the end 13 of the substrate 10. 20

In the above arrangement, all the optical paths 21, 24A, 24B, and 25B lead to the end 13 of the substrate 10, only a single optical fiber array need to be connected.

A third embodiment of the present invention will be described with reference to Fig. 5. Prior 25 to the explanation on the third embodiment, a bandpass filter used in the third embodiment will be described with reference to Fig. 6A to 9B. 25

Figs. 6A to 8B are graphs showing the wavelength characteristics of the band widths when three types of band pass filters Nos. 1 to 3 are inserted in the optical path.

Figs. 6A and 6B, 7A and 7B, and 8A and 8B correspond to filters Nos. 1, 2, and 3, 30 respectively. The layer configurations of the respective filters are as follows: 30

No. 1: HLH(3HLHLHL3H)<sup>3</sup>HLH 23 layers  
 No. 2: HLH(2HLHLHLHL2L)<sup>3</sup>HLH 31 layers  
 No. 3: HLHL(LHLHLHLHL)<sup>2</sup>LHLH 23 layers

35 where H indicates a dielectric layer having a refractive index of 2.2 and a layer thickness corresponding to  $\lambda/4$ , and L indicates a dielectric layer having a reflective index of 1.5 and a layer thickness corresponding to  $\lambda/4$ . Figs. 6A, 7A, and 8A show cases wherein the central wavelength is 900 nm, and Figs. 6B, 7B, and 8B show cases wherein the central wavelength is 40 1,200 nm. The filter angles  $\theta$  defined by the plane normal to the filter and the optical path are  $0^\circ$ ,  $5^\circ$ ,  $10^\circ$ ,  $15^\circ$ , and  $20^\circ$ . The characteristics of the filters having these filter angles are indicated by a solid line, an alternate long and two short dashes line, an alternate long and short dash line, a broken line, and a dotted line in this order. In this embodiment, a buried optical waveguide manufactured by an electric-field assisted 2-step ion exchange process and having a 45 substantially circular section is used. According to the refractive index profile of this optical waveguide, the refractive index is maximum at the central portion and decreases gradually toward the outer surface of the optical waveguide. 45

With filter No. 1, the degradation in maximum transmittance is small and the decrease in transmission band width is also small, while with filters Nos. 2 and 3, both the degradation in 50 maximum transmittance and decrease in transmission band width are large. A required transmission band width depends on the specification of the transmission system. When the variation in wavelength due to temperature change of a light-emitting element to be used and the variation due to the manufacturing condition are taken into account, the band width is preferably about 30 nm or more at a wavelength of 800 to 900 nm, and about 50 nm or more at a wavelength of 55 1,200 to 1,300 nm. Table 1 shows whether the respective filters operating in the waveguide satisfy the above band width conditions when they have a transmittance of 90% or more (a transmittance lower than the maximum transmittance by 10%). 55

Table 1

5	Filter No.	Filter Angle	Wavelength 800 to 900 nm	Wavelength 1,200 to 1,300 nm	5
10	1	10°	Yes	Yes	10
		13°	Yes	Yes	
15	2	10°	No	No	15
		13°	No	No	
20	3	10°	Yes	No	20
		13°	Yes	No	

20 It is found from Table 1 that filter No. 1 is optimal, filter No. 3 is effective only for a wavelength of 800 to 900 nm, and filter No. 2 is not suitable. From Figs. 6A to 8B, the results of Table 1, and other theoretical and experimental studies, it is apparent that, generally, the wider the 90% band width when a filter is arranged in an optical path at a filter angle  $\theta=0^\circ$ , the 25 smaller the degradation in filter characteristics when the filter is arranged at a filter angle  $\theta>0^\circ$ . 25

Table 2 shows whether the 90% transmittance band width becomes 50 nm or more at a wavelength of 800 to 900 nm and 70 nm or more at a wavelength of 1,200 to 1,300 nm when  $\theta=0^\circ$ . 25

30 Table 2

30	Filter No.	Wavelength 800 to 900 nm	Wavelength 1,200 to 1,300 nm	30
35	1	50 nm or more	70 nm or more	35
40	2	less than 50 nm	less than 70 nm	40
40	3	50 nm or more	less than 70 nm	40

Comparison between the results of Tables 1 and 2 shows their correspondence.

From the above results and other studies, it is apparent that, in order to determine whether a certain filter is suitable, the 90% transmittance band width at a filter angle  $\theta=0^\circ$  of a filter in an 45 optical path can be used, and that a suitable filter may hence have a band width of 50 nm or more at a wavelength of 800 to 900 nm and 70 nm or more at a wavelength of 1,200 to 1,300 nm. 45

Regarding the number of layers, a relatively small number of layers of about 23 is appropriate. 50 Figs. 9A and 9B show a relationship between the band width and the transmittance when the angle of filter No. 1 having preferable characteristics is changed. Fig. 9A and 9B show cases wherein the central wavelengths are 900 nm and 1,200 nm, respectively. When the conditions of a band width of 30 nm for the central wavelength 900 nm and that of 50 nm for the central wavelength 1,200 nm are to be satisfied simultaneously, a transmittance of 90% or more cannot be obtained if the filter angle  $\theta \geq 15^\circ$ , while a transmittance of 90% or more can be obtained if 55 the filter angle  $\theta \leq 13^\circ$ . Similarly, a transmittance of 95% or more can be obtained if the filter angle  $\theta \leq 10^\circ$ . However, this range of  $\theta$  is not practical since  $\theta$  becomes a smaller value if another unsuitable filter, e.g., filter No. 2 or 3 described above, is used. 55

From the results of Fig. 9 and other theoretical and experimental studies, it is apparent that the tolerance limit of the filter angle  $\theta$  is  $13^\circ$  from the viewpoint of practical use, and that a filter 60 angle  $\theta \geq 15^\circ$ , as in a conventional demultiplexing and/or multiplexing optical circuit, falls far outside the range to obtain theoretical performance and is thus not preferable at all. 60

Table 3 shows the 90% band width obtainable with filter No. 1 with good characteristics described above. A filter angle  $\theta$  can be determined from Table 3.

Table 3

5	Filter Angle $\theta$	Band Width Central Wavelength		5
		900 nm	1,200 nm	
10	0°	54	71	10
15	5°	50	67	15
20	10°	44	58	20
25	13°	39	52	25
30	15°	36	48	30
35	20°	28	37	35

Fig. 5 is a plan view of a third embodiment of the present invention. Optical paths 60 to 67 for constituting a buried-type optical waveguide are formed in a predetermined circuit pattern in a glass plate substrate 10. Grooves 70 to 72 are formed at respective portions of the surface of the substrate 10 to cross the optical waveguide. Interference filter groups 90 to 93 are fitted in the grooves 70 to 72, respectively.

The substrate 10 is made of a glass containing, e.g.,  $\text{SiO}_2$  and  $\text{B}_2\text{O}_3$  as major matrix forming oxides and a small amount of alkali ions for ion exchange. A mask having an aperture corresponding to the predetermined circuit pattern is formed on the glass substrate 10 by photolithography or the like. Ions having a valence of 1, e.g.,  $\text{Tl}^+$ , which contribute to the increase in refractive index of glass, are diffused through the mask aperture by the first ion exchange with the alkali ions in an electric field. Ions which contribute to the decrease in refractive index of the glass are diffused by the second ion exchange. The optical paths 60 to 67 are thus formed.

The optical paths 60 to 67 formed in the above method have substantially circular sections and refractive index profiles wherein a refractive index decreases gradually from the center to the outer surface of the respective optical path. These optical paths 60 to 67 are coupled with optical fibers at a low coupling loss.

The grooves 70 to 72 are formed to be substantially parallel to the ends of the substrate 10 and have, e.g., a width of about 40  $\mu\text{m}$  and a depth of about 200  $\mu\text{m}$ .

The optical paths 61 and 63 intersect each other at the groove 72 at an incident angle  $\theta=10^\circ$ . The optical paths 63 and 66 intersect each other at the groove 71 at an incident angle  $\theta=10^\circ$ . The left hand portions of the optical paths 61 and 64 and the right hand portions of the optical paths 62 and 66 are substantially parallel to the longer sides of the substrate 10. The right- and left hand portions of the optical paths 61 and 62 extend substantially linearly. The optical path 63 and the right hand portion of the optical path 64 extend substantially linearly.

A short-wavelength pass filter 90 is inserted in a portion of the groove 72 at which the ends of the optical paths 61 to 63 are located. A bandpass filter 92 is inserted between the optical paths 66 and 67. A bandpass filter 91 is inserted at a portion of the groove 71 at which the ends of the optical paths 63, 64, and 66 are located. A bandpass filter 93 is inserted at a portion of the groove 70 at which the end of the optical path 64 is located.

The short-wavelength pass filter 90 and the band pass filters 91 to 93 are thin plates having thicknesses of not more than 40  $\mu\text{m}$  and are fixed in the grooves 70 to 72 by an optical adhesive. The short-wavelength pass filter 90 has a high transmittance for the entire wavelength range of 800 and 900 nm and has a rejection band attenuation of 30 dB or more for a wavelength of 1,200 to 1,300 nm. The short-wavelength pass filter 90 is used to divide only a component of wavelength 1 from a mixed beam having components of wavelengths of  $\lambda_1=890$  nm,  $\lambda_2=1,200$  nm, and  $\lambda_3=1,300$  nm that propagate through the optical paths 60 and 61. The component of wavelength  $\lambda_1$  is guided to the optical path 62. The bandpass filter 91 is used for demultiplexing the components of wavelengths  $\lambda_2$  and  $\lambda_3$ . In this case, in order to obtain desired demultiplexing characteristics, filter No. 1 described above is used at a filter angle  $\theta=10^\circ$ .

Filter No. 1 was manufactured to have a central wavelength of  $\lambda_3$  and a configuration as described above. The refractive indexes of the H and L layers were set to 2.2 and 1.5, respectively.  $\text{TiO}_2$  was used as a deposition material for an H layer. Manufacturing conditions shown as a deposition rate and a substrate temperature were optimized so that the H layer had the refractive index of 2.2 which is lower than that of a bulk substrate. In this case, a band

width of 55 nm or more was obtained at a transmittance of 92%, and the rejection band attenuation for a wavelength deviated from a central wavelength by 100 nm was 28 dB.

The bandpass filters 92 and 93 are used for passing components having central wavelengths of 2 and  $\lambda_3$ , and the angle of incidence of the beams on the filters 92 and 93 is 90°. Since the filter angle  $\theta$  of the filters 92 and 93 is  $\theta=0^\circ$ , the degradation in characteristics due to the increase in angle of the incident light is very small and does not depend so much on the layer configuration of each filter. 5

The band pass filters 92 and 93 were filters which had a transmission band width of 60 to 10 65 nm at a transmittance of 95% and their rejection band attenuation for a wavelength deviated from a central wavelength by 100 nm was 30 dB. The filter angles  $\theta$  of the bandpass filters 92 and 93 can be other than 0°. However,  $\theta \leq 7^\circ$  is preferable in order to prevent a decrease in 10 band width. Optical adhesives 80 and 81 fill portions of the grooves 70 and 71 at which the optical paths 60 and 61 are located so as to prevent light leakage losses by separation of the optical paths 60 and 61. 10

15 In the third embodiment, when mixed a beam including components at three wavelengths of  $\lambda_1$ ,  $\lambda_2$ , and  $\lambda_3$  is incident on the input optical path 20, a component of wavelength  $\lambda_1$  passes through the short-wavelength pass filter 90 and is guided to the output optical path 62. The components at wavelengths  $\lambda_2$  and  $\lambda_3$  are reflected by the filter 90, propagate in the optical path 63, and reach the bandpass filter 91. Of these components, the component at wavelength 20  $\lambda_2$  is reflected by the filter 91, propagates through the optical path 66, passes through the bandpass filter 92, and is output from the end of the output optical path 67. The component at wavelength  $\lambda_3$  passes the filter 91 and the bandpass filter 93 and is output from the end of the output optical path 65 to outside the substrate 10. 15

In this manner, the beam of mixed wavelengths of  $\lambda_1$ ,  $\lambda_2$ , and  $\lambda_3$  is guided into the different 25 optical paths 62, 67, and 65 depending on the wavelengths. 25

In the third embodiment, the insertion losses of the respective channels were 2 dB or less for the central wavelengths  $\lambda_1$ ,  $\lambda_2$ , and  $\lambda_3$  and were 2.5 dB or less for the entire band width (35 nm for the channel of the wavelength  $\lambda_1$  and 55 nm for the channels of the wavelengths  $\lambda_2$  and  $\lambda_3$ ). The far-end crosstalk attenuation was 30 dB for the channel for wavelength  $\lambda_1$ , 45 dB for 30 the channel of wavelength  $\lambda_2$ , and 60 dB or more for the channel of wavelength  $\lambda_3$ . 30

In the above explanation, the function of the third embodiment used as a demultiplexing optical circuit is described. The optical circuit of the third embodiment can be used as a multiplexing optical circuit or a bidirectional demultiplexing and/or multiplexing optical circuit. In the latter case, the near-end crosstalk attenuation was 70 dB or more for the respective channels. 35

35 When the optical circuit of the third embodiment is used as a multiplexing optical circuit or a demultiplexing and/or multiplexing optical circuit, the filter 92 or 93 other than the filters 90 and 91 for performing demultiplexing by transmittance or reflection can be omitted as needed.

In the above embodiment of demultiplexing and/or multiplexing optical circuit the axis of the filter-fitting groove is perpendicular to the side of the substrate. Therefore, a plurality of optical 40 waveguides having the same circuit patterns can be formed in a large substrate base to be adjacent to each other. Grooving may then be performed in a single operation at a predetermined portion of the base. Then, the substrate may be cut to produce a plurality of demultiplexing and/or multiplexing optical circuits having predetermined filter-fitting grooves. 40

Therefore, the simultaneous manufacture of a plurality of demultiplexer and/or multiplexers, 45 which is impossible with conventional demultiplexers and/or multiplexers, can be easily accomplished. Furthermore, since the groove for receiving the filter is perpendicular to the side of the substrate it is relatively easy to ensure high machining precision. 45

#### CLAIMS

50 1. A demultiplexing and/or multiplexing optical circuit comprising a substrate having two opposed parallel edge regions, an optical waveguide formed in said substrate and including a branched portion for dividing an incident optical path into a transmitting optical path and a reflecting optical path, a groove formed in said substrate in a direction perpendicular to said edge regions and disposed to cross said optical waveguide at said branched portion and at a portion partway along one of said optical paths, and a plurality of filters located in said groove. 50

55 2. A circuit according to claim 1, wherein said optical waveguide has a circuit pattern such that at least one of said branching portions and at least one of said optical paths commonly use said groove.

3. A circuit according to claim 1, wherein said optical waveguide has a circuit pattern such 60 that all of said filters required in said waveguide are received in a single groove extending perpendicular to said edge regions. 60

4. A circuit according to any one of claims 1 to 3, wherein the substrate includes two end regions generally perpendicular to said edge regions and an optical path obliquely intersects said groove, and is provided with at least one arcuate bent portion whereby the optical axis of said 65 optical path at and adjacent each end of said substrate is perpendicular to each end of the 65

substrate.

5. A circuit according to any one of claims 1 to 4, wherein half of the angle defined between said incident optical path and said reflecting optical path is not more than 13°.

6. A circuit according to any one of claims 1 to 5, wherein at least one of said filters is a 5 bandpass filter having a 90% transmittance band width of not less than 50 nm for a wavelength of 800 to 900 nm and not less than 70 nm for a wavelength of 1,200 to 1,300 nm in a state wherein said filter is inserted into an optical waveguide with its normal coincident with the optical axis of said optical path.

7. A circuit according to any one of claims 1 to 6, wherein at least one of said filters has a 10 23-layer structure indicated by  $HLH(3HLHLHL3H)^3HLH$  where H is a layer having a relatively high refractive index and a layer thickness corresponding to  $\lambda/4$  and L is a layer having a relatively low refractive index and a layer thickness corresponding to  $\lambda/4$ .

8. A circuit according to any one of claims 1 to 7, wherein said optical path has a refractive index gradient in a radial direction within a section thereof.

15 9. A circuit substantially as hereinbefore described with reference to and as illustrated in any of Figs. 2 to 9 of the accompanying drawings. 15

Printed for Her Majesty's Stationery Office by Burgess & Son (Abingdon) Ltd, Dd 8991685, 1987.  
Published at The Patent Office, 25 Southampton Buildings, London, WC2A 1AY, from which copies may be obtained.